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Modelling and simulation of interactions of reactive flow with a solid structure leading to volume changes Application to plaque formations in arteries

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University Partnership Heidelberg-Prague Celebrating twenty-five years of successful cooperation 27th-29th April, 2015, Prague

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• The interaction of reactive flow with a solid structure is an important aspect in various applications.

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- The interaction of reactive flow with a solid structure is an important aspect in various applications.
- Penetration of chemical substances from the flow into the solid phase leads to changes in volume of the solid.



#### Volume Changes



- $\Omega_f^t$ : the fluid domain;  $\Omega_s^t$ : the solid domain.
- $\Gamma_1^t \cup \Gamma_2^t$ : the interface between  $\Omega_f^t$  and  $\Omega_s^t$ .  $\Gamma_1^t$  is permeable to chemical substances.
- Chemical substances migrate through  $\Gamma_1^t$  from  $\Omega_f^t$  into  $\Omega_s^t$ . Their accumulation and chemical reactions lead to volume growth of  $\Omega_s^t$ .

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• The interaction of reactive flow with a solid structure is an important aspect in various applications.

- Penetration of chemical substances from the flow into the solid phase leads to changes in volume of the solid.
- This type of processes occurs e.g. in plaque formation in arteries.

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## Processes to be modeled

- Main processes of such interaction can be categorized as either biomechanical or biochemical.
  - Biomechanical processes: fluid-structure interaction between reactive flow and solid structure.
  - Biochemical processes: transport and reactions of chemical substances.
- The problems of biomechanical and biochemical processes are coupled with growth modeling.

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#### Processes to be modeled

#### • Main variables:

- *p*: pressure (both in  $\Omega_f^t$  and  $\Omega_s^t$ )  $\rho$ : density (in  $\Omega_s^t$ )
- v: velocity (both in Ω<sup>t</sup><sub>f</sub> and Ω<sup>t</sup><sub>s</sub>)
   u: displacement (in Ω<sup>t</sup><sub>s</sub>)
- c<sub>1,f</sub>, c<sub>2,f</sub>, ..., c<sub>n,f</sub>: concentrations of chemical substances (in Ω<sup>t</sup><sub>f</sub>)
- c<sub>1,s</sub>, c<sub>2,s</sub>, ..., c<sub>m,s</sub>: concentrations of chemical substances (in Ω<sup>t</sup><sub>s</sub>)
- g: metric of growth(in Ω<sup>t</sup><sub>s</sub>)
- All the variables are distinguished by lower indexes "f" and "s" in Ω<sup>t</sup><sub>f</sub> and Ω<sup>t</sup><sub>s</sub>.
- All the equations are derived in Eulerian coordinate.

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## Derivation of the Equations

#### Fluid-Structure Interaction Problem

• The fluid dynamics (incompressible fluid):

$$divv_f = 0 \quad \text{in} \quad \Omega_f^t$$
$$\rho_f \partial_t v_f + \rho_f v_f \cdot \nabla v_f = div\sigma_f \quad \text{in} \quad \Omega_f^t$$

• The structural mechanics (elastic material):

$$\partial_t \rho_s + div(\rho_s v_s) = f_s^g \quad \text{in} \quad \Omega_s^t$$
$$\rho_s \partial_t v_s + \rho_s v_s \cdot \nabla v_s = div\sigma_s \quad \text{in} \quad \Omega_s^t$$
$$\partial_t u_s + v_s \cdot \nabla u_s = v_s \quad \text{in} \quad \Omega_s^t$$

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## Derivation of the Equations

#### **Reactive Transport Problem**

Motion of chemical substances in Ω<sup>t</sup><sub>f</sub>:

$$\partial_t c_{i,f} + div(c_{i,f}v_f) - D_{i,f} \triangle c_{i,f} = 0$$
 in  $\Omega_f^t$ ,  $i = 1, 2, ..., n$ 

Motion of chemical substances in Ω<sup>t</sup><sub>s</sub>:

$$\partial_t c_{j,s} + div(c_{j,s}v_f) - div(D_{j,s}\nabla c_{j,s}) = f_{j,s}^r \quad \text{in} \quad \Omega_s^t, \quad j = 1, 2, ..., m$$

Reaction functions:

$$f_{j,s}^r = f_{j,s}^r(c_{1,s}, c_{2,s}, ..., c_{m,s}) \quad j = 1, 2, ..., m$$

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# Derivation of the Equations

#### The stress tensor $\sigma_s$

•  $\sigma_s$  is determined by the deformation gradient  $F_s$ :

$$\sigma_s = \sigma_s(F_s), \ F_s = ?$$



Growth may falsify the usual way of quantifying the deformation.

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# Derivation of the Equations

#### The decomposition of deformation gradient



- $\Omega_t^N$ : the natural configuration of the domain at time t
- *F<sub>s</sub>* is decomposed in a product of corresponding tensors *G<sub>s</sub>* and *F<sup>e</sup><sub>s</sub>*.

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#### Derivation of the Equations

#### Growth modeling

• The growth matrix:

$$F_s = F_s^e \cdot G_s, G_s = g_s I$$
$$\sigma_s = \sigma_s (F_s^e)$$

• The metric of growth:

$$d\partial_t g_s + dv_s \cdot \nabla g_s = \frac{f_s^g}{\rho_s} g_s$$
 in  $\Omega_s^0$ 

Growth function:

$$f_s^g = f_s^g(f_{1,s}^r, f_{2,s}^r, ..., f_{m,s}^r)$$

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# Atherosclerotic Plaque Formation

• Plaque formation is induced by penetration of monocytes. The growth and rupture of plaque is one of the main causes for blockage of a main artery which can lead to ischaemic brain infarct, heart attack and some other cardiovascular diseases.



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#### Atherosclerotic Plaque Formation



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Hahn and Schwartz, Nature Reviews 10:53-62, 2009

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## Atherosclerotic Plaque Formation



- Foam cells form a lipid core surrounded by a fibrous cap formed by smooth muscle cells, narrowing the vessel lumen and making the plaque be vulnerable.
- If plaque rupture happens on the fibrous cap, an occlusive thrombus will be superimposed on the plaque to block the vessel.

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## Mathematical Model

- Ω<sup>t</sup><sub>f</sub> is occupied by blood flow.
- Ω<sup>t</sup><sub>s</sub> is occupied by vessel wall.
- · Chemical substances:
  - $c_f$ : concentration of monocytes (in  $\Omega_f^t$ )
  - c<sub>s</sub>: concentration of macrophages (in Ω<sup>t</sup><sub>s</sub>)
  - c<sup>\*</sup><sub>s</sub>: concentration of foam cells (in Ω<sup>t</sup><sub>s</sub>)
- All the equations are derived in Eulerian coordinate in Ω<sup>t</sup><sub>f</sub> and in Lagrangian coordinate in Ω<sup>0</sup><sub>s</sub>.

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## **Mathematical Model**

• Fluid-structure interaction problem:

$$divv_{f} = 0 \quad \text{in} \quad \Omega_{f}^{t}$$

$$\rho_{f}\partial_{t}v_{f} + \rho_{f}v_{f} \cdot \nabla v_{f} = div\sigma_{f} \quad \text{in} \quad \Omega_{f}^{t}$$

$$\hat{J}_{s}\hat{\rho}_{s}\partial_{t}\hat{v}_{s} = \widehat{div}(\hat{J}_{s}\hat{\sigma}_{s}\hat{F}_{s}^{-T}) \quad \text{in} \quad \Omega_{s}^{0}$$

$$\partial_{t}\hat{u}_{s} = \hat{v}_{s} \quad \text{in} \quad \Omega_{s}^{0}$$

• Reactive transport problem:

$$\partial_t c_f + v_f \cdot \nabla c_f - D_f \triangle c_f = 0 \quad \text{in} \quad \Omega_f^t$$
$$\partial_t (\hat{J}_s \hat{c}_s) - \widehat{div} (\hat{J}_s \hat{F}_s^{-1} \hat{D}_s \hat{F}_s^{-T} \hat{\nabla} \hat{c}_s) = - \hat{J}_s \hat{f}_s^r \quad \text{in} \quad \Omega_s^0$$
$$\partial_t (\hat{J}_s \hat{c}_s^*) = \hat{J}_s \hat{f}_s^r \quad \text{in} \quad \Omega_s^0.$$

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# Mathematical Model

• The metric of growth:

$$d\partial_t \hat{g}_s = \frac{\hat{f}_s^g}{\hat{\rho}_s} \hat{g}_s$$
 in  $\Omega_s^0$ 

Growth function:

$$\hat{f}^g_s = \hat{f}^g_s(\hat{f}^r_s)$$

Reaction functions:

$$\hat{f}_s^r = \hat{f}_s^r(\hat{c}_s)$$

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#### Mathematical Model

Constitutive equations:

$$\begin{split} \sigma_f &= -p_f I + \rho_f v (\nabla v_f + \nabla v_f^T) \quad (\text{Navier-Stokes}) \quad \text{in} \quad \Omega_f^t \\ \hat{\sigma}_s &= -\hat{p}_s I + \hat{\mu}_s (\hat{F}_s^e \hat{F}_s^{eT} - I) \quad (\text{incompressible neo-Hookean}) \quad \text{in} \quad \Omega_s^0 \\ \hat{F}_s^e &= \hat{F}_s \hat{G}_s^{-1} = \frac{1}{\hat{g}_s} \hat{F}_s \quad \text{in} \quad \Omega_s^0 \end{split}$$

• Transmission conditions on the interface:

$$\sigma_f \cdot n_f + \sigma_s \cdot n_s = 0, \quad v_f = v_s \quad \text{on} \quad \Gamma_1^t \cup \Gamma_2^t$$
$$D_f \nabla c_f \cdot n_f + D_s \nabla c_s \cdot n_s = 0 \quad \text{on} \quad \Gamma_1^t \cup \Gamma_2^t$$
$$D_f \nabla c_f \cdot n_f + \zeta(c_f - c_s) = 0 \quad \text{on} \quad \Gamma_1^t \cup \Gamma_2^t$$

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# **Numerical Simulation**

- Main difficulty of Numerics:
  - The equations are formulated in different coordinates (Eulerian coordinate in Ω<sup>t</sup><sub>f</sub> and Lagrangian coordinate in Ω<sup>0</sup><sub>s</sub>).
  - Some of the equations are formulated in the moving domain  $\Omega_f^t$ , so we need different meshes at each time step.
- The clue to treat this problem is to formulate the systems in one common coordinate: Arbitrary Lagrangian Eulerian(ALE) Coordinate.
  - All the equations are rewritten in the fixed domain Ω<sup>0</sup><sub>f</sub> or Ω<sup>0</sup><sub>s</sub>.
  - The construction of the ALE mapping in Ω<sup>0</sup><sub>f</sub> is obtained in terms of the artificial variable û<sub>f</sub>, which is defined by harmonic extension.

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# **Numerical Simulation**

#### Variational formulation in ALE Coordinate

• Fluid-structure interaction problem:

 $(\hat{J}\hat{\rho}_f(\partial_t\hat{v}+\hat{F}^{-1}(\hat{v}-\partial_t\hat{u})\cdot\hat{\nabla}\hat{v}),\hat{\phi}^{\nu})_{\Omega^0_{\varepsilon}}+(\hat{J}\hat{\rho}_s\partial_t\hat{v},\hat{\phi}^{\nu})_{\Omega^0_{\varepsilon}}$  $+ (\hat{J}\hat{\sigma}_{f}\hat{F}^{-T},\hat{\nabla}\hat{\phi}^{\nu})_{\Omega^{0}_{\epsilon}} + (\hat{J}\hat{\sigma}_{s}\hat{F}^{-T},\hat{\nabla}\hat{\phi}^{\nu})_{\Omega^{0}_{\epsilon}} = \langle \hat{g}_{f}^{out},\hat{\phi}^{\nu} \rangle_{\Gamma_{f,out}}$  $(\hat{div}(\hat{J}\hat{F}^{-1}\hat{v}),\hat{\phi}^{p})_{\Omega^{0}_{\epsilon}} + (\hat{J}^{e}_{s} - 1,\hat{\phi}^{p})_{\Omega^{0}_{s}} = 0$  $\alpha(\hat{\nabla}\hat{u},\hat{\nabla}\hat{\phi}^{u})_{\Omega^{0}_{c}}+(\partial_{t}\hat{u}-\hat{v},\hat{\phi}^{u})_{\Omega^{0}_{c}}=0$  $\hat{\sigma}_f = -\hat{p}I + \hat{\rho}_f \nu (\hat{\nabla}\hat{\nu}\hat{F}^{-1} + \hat{F}^{-T}\hat{\nabla}\hat{\nu}^T)$  $\hat{\sigma}_{s} = -\hat{p}_{s}I + \hat{\mu}_{s}(\hat{F}_{s}^{e}\hat{F}_{s}^{eT} - I)$  $\hat{g}_f^{out} = \hat{J}\hat{\rho}_f v \hat{F}^{-T} \hat{\nabla} \hat{v}^T \hat{F}^{-T}$ 

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# Numerical Simulation

• Reactive transport problem:

 $\begin{aligned} (\hat{J}\partial_{t}\hat{c}_{f},\hat{\phi}_{f}^{c})_{\Omega_{f}^{0}} + (\hat{J}\hat{F}^{-1}(\hat{v}-\partial_{t}\hat{u})\cdot\hat{\nabla}\hat{c}_{f},\hat{\phi}_{f}^{c})_{\Omega_{f}^{0}} + (\hat{J}D_{f}\hat{F}^{-T}\hat{\nabla}\hat{c}_{f},\hat{F}^{-T}\hat{\nabla}\hat{\phi}_{f}^{c})_{\Omega_{f}^{0}} \\ &= \langle \zeta(\hat{c}_{f}-\hat{c}_{s})\hat{J}|\hat{F}^{-T}\cdot N_{f}|,\hat{\phi}_{f}^{c}\rangle_{\Gamma_{1}^{0}\cup\Gamma_{2}^{0}} \\ (\partial_{t}(\hat{J}\hat{c}_{s}),\hat{\phi}_{s}^{c})_{\Omega_{s}^{0}} + (\hat{J}\hat{D}_{s}\hat{F}^{-T}\hat{\nabla}\hat{c}_{s},\hat{F}^{-T}\hat{\nabla}\hat{\phi}_{s}^{c})_{\Omega_{s}^{0}} + (\hat{J}\hat{f}_{s}^{r},\hat{\phi}_{s}^{c})_{\Omega_{s}^{0}} \\ &= \langle \zeta(\hat{c}_{s}-\hat{c}_{f})\hat{J}|\hat{F}^{-T}\cdot N_{s}|,\hat{\phi}_{s}^{c}\rangle_{\Gamma_{1}^{0}\cup\Gamma_{2}^{0}} \\ (\partial_{t}(\hat{J}\hat{c}_{s}^{*}),\hat{\phi}_{s}^{c*})_{\Omega_{s}^{0}} - (\hat{J}\hat{f}_{s}^{r},\hat{\phi}_{s}^{c*})_{\Omega_{s}^{0}} = 0 \end{aligned}$ 

• Metric of growth:

$$(d\hat{\rho}_s\partial_t\hat{g}_s,\hat{\phi}_s^g)_{\Omega_s^0} - (\hat{f}_s^g\hat{g}_s,\hat{\phi}_s^g)_{\Omega_s^0} = 0$$

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# Numerical Methods

 Numerical simulations are performed by using Gascoigne, the software developed by the Numerical Methods Group in IWR, Heidelberg University.



- The time discretization is achieved with implicit backward Euler scheme.
- The spatial discretization is based on the Galerkin finite element method.
- The nonlinear problems are linearized and solved by Newton method.

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#### Numerical Results

#### Initial Computational Domain



- The upper dashed line Γ<sub>1</sub><sup>0</sup> denotes the interface permeable for monocytes.
- The layer  $\Omega_s^e$  between two dashed lines represents the endothelial cells and smooth muscle cells, where chemical reactions rarely take place.

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**Numerical Results** 

• Distribution of velocity in *x*-direction and motion of the interface

t = 0max  $v_x = 300 mm/s$ 

 $t = 4.5 \times 10^7$  seconds  $\approx 521$  days max  $v_x = 334.51$  mm/s



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### **Numerical Results**

Distribution of displacement in y-direction in Ω<sup>t</sup><sub>s</sub>

t = 0max  $u_{s,y} = 0mm$ 

 $t = 4.5 \times 10^7$  seconds  $\approx 521$  days  $max u_{s,y} = 0.92mm$ 



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# **Numerical Results**

Distribution of concentration of monocytes in Ω<sup>t</sup><sub>f</sub>







 $t = 4.5 \times 10^7$  seconds  $\approx 521$  days

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## **Numerical Results**

Distribution of concentration of foam cells in Ω<sup>t</sup><sub>s</sub>

t = 0max  $c_s^* = 0/mm^3$ 

 $t = 4.5 \times 10^7$  seconds  $\approx 521$  days  $max c_s^* = 1393/mm^3$ 



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#### **Numerical Results**

Distribution of principal stress in Ω<sup>t</sup><sub>s</sub>

$$t = 0$$
  
max  $\sigma_{s,p} = 0g/mm \cdot s^2$ 

 $t = 4.5 \times 10^7$  seconds  $\approx 521$  days  $max \sigma_{s,p} = 2662.98g/mm \cdot s^2$ 



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# **Conclusion and Outlook**

- We treat a mathematical model consisting of a fluid-structure interaction problem coupled with a reactive transport problem.
- This model is used to describe plaque formation, and the numerical results are in good agreement with observations.
  - The penetration of monocytes and accumulation of foam cells lead to the formation and growth of plaques.
  - The formation and evolution of plaques induces the increase of stresses in the vessel wall, which is an indicator of plaque rupture.
- More realistic description of the vessel wall including the oscillation of blood flow and parameter estimation from real data will be considered.

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# Thank You!

