hp-Version Trefftz Discontinuous Galerkin Method for the Homogeneous Helmholtz Equation

Scott Congreve

Fakultät für Mathematik, Universität Wien

Joint work with Ilaria Perugia (Universität Wien) Paul Houston (University of Nottingham)

Austrian Numerical Analysis Day 2016



Helmholtz Equation

2 Trefftz DG Spaces

Comparison to Polynomial DG

3 Derivation of Trefftz DG

Selection of Flux Parameter

- A priori Error Estimates
- Comparison of Flux Parameters
- 9 Plane Wave Direction Refinement

6 Adaptive Refinement

A posteriori Error Estimates



Let $\Omega \subset \mathbb{R}^d$, d = 2, 3 be a bounded polygonal/polyhedral domain.

$-\Delta u - k^2 u = 0$	in Ω ,
<i>u</i> = 0	on Γ_D ,
$ abla u \cdot \boldsymbol{n} = 0$	on Γ_N ,
$ abla u \cdot \mathbf{n} + ik \vartheta u = g_R$	on Γ_R .

(sound-soft scattering) (sound-hard scattering)





Sound-hard Scattering

Acoustic Wave Prop.

Sound-soft Scattering



Problems with FEM:

- Number of *degrees of freedom* required to obtain given accuracy increases with wave number *k*.
- *h*-version FEM affected by pollution effect [Babuška & Sauter, 2000]:

$$\|u-u_h\| \leq \frac{C(k)}{v_h \in V(\mathcal{T}_h)} \|u-v_h\|$$

C(k) is an increasing function in k.



Problems with FEM:

- Number of *degrees of freedom* required to obtain given accuracy increases with wave number k.
- h-version FEM affected by pollution effect [Babuška & Sauter, 2000]:

$$\|u-u_h\| \leq \frac{\mathcal{C}(k)}{v_h \in V(\mathcal{T}_h)} \|u-v_h\|$$

C(k) is an increasing function in k.

We incorporate information about the frequency into the finite element space to attempt to reduce computation cost.

Trefftz FEM Spaces



Polynomial DG Finite Element Spaces: DGFEM uses polynomial basis functions defined on a reference element \hat{K} :

$$V_q^{DG}(\mathcal{T}_h) \coloneqq \{ v \in L^2(\Omega) : v |_{\mathcal{K}} \circ F_{\mathcal{K}} \in \mathcal{S}_{q_{\mathcal{K}}}(\widehat{\mathcal{K}}), \mathcal{K} \in \mathcal{T}_h \}.$$

Trefftz FEM Spaces



Polynomial DG Finite Element Spaces: DGFEM uses polynomial basis functions defined on a reference element \widehat{K} :

$$V_q^{DG}(\mathcal{T}_h) \coloneqq \{ v \in L^2(\Omega) : v |_{\mathcal{K}} \circ F_{\mathcal{K}} \in \mathcal{S}_{q_{\mathcal{K}}}(\widehat{\mathcal{K}}), \mathcal{K} \in \mathcal{T}_h \}.$$

Trefftz Finite Element Space: Use basis functions defined element-wise based on general solutions to the PDE. First define the local Trefftz spaces

$$T(K) \coloneqq \{v|_K : -\Delta u - k^2 u = 0\}$$

and let

$$T(\mathcal{T}_h) \coloneqq \{ v \in L^2(\Omega) : v |_{\mathcal{K}} \in T(\mathcal{K}), \mathcal{K} \in \mathcal{T}_h \}.$$

Trefftz FEM Spaces



Polynomial DG Finite Element Spaces: DGFEM uses polynomial basis functions defined on a reference element \widehat{K} :

$$V_q^{DG}(\mathcal{T}_h) \coloneqq \{ v \in L^2(\Omega) : v|_{\mathcal{K}} \circ F_{\mathcal{K}} \in \mathcal{S}_{q_{\mathcal{K}}}(\widehat{\mathcal{K}}), \mathcal{K} \in \mathcal{T}_h \}.$$

Trefftz Finite Element Space: Use basis functions defined element-wise based on general solutions to the PDE. First define the local Trefftz spaces

$$T(K) \coloneqq \{v|_K : -\Delta u - k^2 u = 0\}$$

and let

$$T(\mathcal{T}_h) \coloneqq \{ v \in L^2(\Omega) : v |_{\mathcal{K}} \in T(\mathcal{K}), \mathcal{K} \in \mathcal{T}_h \}.$$

We let $V_p(K) \subset T(K)$ be a finite dimensional local space; then, the Trefftz FE Space is given by

$$V_p(\mathcal{T}_h) \coloneqq \{ v \in T(\mathcal{T}_h) : v_K \in V_p(K), K \in \mathcal{T}_h \}.$$

Plane Waves



$$V_{p}(K) = \left\{ v : v(\mathbf{x}) = \sum_{\ell=1}^{p_{K}} \alpha_{\ell} e^{ik\mathbf{d}_{\ell} \cdot (\mathbf{x} - \mathbf{x}_{K})}, \alpha_{\ell} \in \mathbb{C} \right\}$$

where p_K is the number of *degrees of freedom* for the element K, d_I , $I = 1, \dots, N_K$ are p_K (roughly) evenly spaced unit direction vectors, and x_K is the centre of the element.

Plane Waves



$$V_{p}(K) = \left\{ v : v(\mathbf{x}) = \sum_{\ell=1}^{p_{K}} \alpha_{\ell} e^{ik\mathbf{d}_{\ell} \cdot (\mathbf{x} - \mathbf{x}_{K})}, \alpha_{\ell} \in \mathbb{C} \right\}$$

where p_K is the number of *degrees of freedom* for the element K, d_I , $I = 1, \dots, N_K$ are p_K (roughly) evenly spaced unit direction vectors, and x_K is the centre of the element.

Trefftz DG has less degrees of freedom than high-order polynomials for the same accuracy.

Number of Degrees of Freedom

Plane Waves

$$V_{p}(K) = \left\{ v : v(\boldsymbol{x}) = \sum_{\ell=1}^{p_{K}} \alpha_{\ell} e^{ik\boldsymbol{d}_{\ell} \cdot (\boldsymbol{x} - \boldsymbol{x}_{K})}, \alpha_{\ell} \in \mathbb{C} \right\}$$

where p_K is the number of *degrees of freedom* for the element K, d_I , $I = 1, \dots, N_K$ are p_K (roughly) evenly spaced unit direction vectors, and x_K is the centre of the element.

Trefftz DG has less degrees of freedom than high-order polynomials for the same accuracy.



Number of Degrees of Freedom



Direction Vectors



[Sloan & Womersley, 2004]



Consider the smooth (analytic) solution (for Acoustic Wave Propagation)

 $u(r,\theta) = \mathcal{J}_1(kr)\cos(\theta)$

for k=20 on the domain $\Omega=(0,1) imes(-1/2,1/2).$



Analytical Solution (Real Part)



Consider the smooth (analytic) solution (for Acoustic Wave Propagation)

 $u(r,\theta) = \mathcal{J}_1(kr)\cos(\theta)$

for k = 20 on the domain $\Omega = (0, 1) \times (-1/2, 1/2)$. We solve using both a DGFEM (solid line) and Trefftz DGFEM (dashed).



(Real Part)





Consider the smooth (analytic) solution (for Acoustic Wave Propagation)

 $u(r,\theta) = \mathcal{J}_1(kr)\cos(\theta)$

for k = 20 on the domain $\Omega = (0, 1) \times (-1/2, 1/2)$.

We solve using both a DGFEM (solid line) and Trefftz DGFEM (dashed).





Consider the smooth (analytic) solution (for Acoustic Wave Propagation)

 $u(r,\theta) = \mathcal{J}_1(kr)\cos(\theta)$

for k = 20 on the domain $\Omega = (0, 1) \times (-1/2, 1/2)$.

We solve using both a DGFEM (solid line) and Trefftz DGFEM (dashed).





Given a mesh \mathcal{T}_h on Ω we derive the TDGFEM as follows.

0



Given a mesh \mathcal{T}_h on Ω we derive the TDGFEM as follows.

$$\int_{\mathcal{K}} (-\Delta u - k^2 u) \, \overline{\mathbf{v}} \quad d\mathbf{x} = 0$$



Given a mesh \mathcal{T}_h on Ω we derive the TDGFEM as follows.

$$\int_{\mathcal{K}} (\nabla u \cdot \nabla \bar{v} - k^2 u \bar{v}) \, d\mathbf{x} \qquad - \int_{\partial \mathcal{K}} \nabla u \cdot \mathbf{n}_{\mathcal{K}} \bar{v} \, ds = 0$$



Given a mesh \mathcal{T}_h on Ω we derive the TDGFEM as follows.

$$\int_{K} u(-\Delta \bar{v} - k^{2} \bar{v}) d\mathbf{x} + \int_{\partial K} u \nabla \bar{v} \cdot \mathbf{n}_{K} ds - \int_{\partial K} \nabla u \cdot \mathbf{n}_{K} \bar{v} ds = 0$$



Given a mesh \mathcal{T}_h on Ω we derive the TDGFEM as follows.

$$\int_{K} u(-\Delta \bar{v} - k^{2} \bar{v}) d\mathbf{x} + \int_{\partial K} u \nabla \bar{v} \cdot \mathbf{n}_{K} ds - \int_{\partial K} \nabla u \cdot \mathbf{n}_{K} \bar{v} ds = 0$$



Given a mesh \mathcal{T}_h on Ω we derive the TDGFEM as follows.

Multiply by test functions and integrate by parts, element-wise, twice (ultra weak formulation):

$$\int_{K} u(-\Delta \bar{v} - k^{2} \bar{v}) d\mathbf{x} + \int_{\partial K} u \nabla \bar{v} \cdot \mathbf{n}_{K} ds - \int_{\partial K} \nabla u \cdot \mathbf{n}_{K} \bar{v} ds = 0$$

Replace continuous functions by discrete approximations $(u_{hp}, v_{hp} \in V_p(\mathcal{T}_h))$ and traces by numerical fluxes

$$u \to \widehat{u}_{hp}, \qquad \nabla u \to ik\widehat{\sigma}_{hp}.$$



Given a mesh \mathcal{T}_h on Ω we derive the TDGFEM as follows.

Multiply by test functions and integrate by parts, element-wise, twice (ultra weak formulation):

$$\int_{K} u(-\Delta \bar{v} - k^{2} \bar{v}) d\mathbf{x} + \int_{\partial K} u \nabla \bar{v} \cdot \mathbf{n}_{K} ds - \int_{\partial K} \nabla u \cdot \mathbf{n}_{K} \bar{v} ds = 0$$

Replace continuous functions by discrete approximations $(u_{hp}, v_{hp} \in V_p(\mathcal{T}_h))$ and traces by numerical fluxes

$$u o \widehat{u}_{hp}, \qquad \nabla u o ik\widehat{\sigma}_{hp}.$$

•
$$v \in V_p(\mathcal{T}_h) \subset T(\mathcal{T}_h) \implies -\Delta \bar{v} - k^2 \bar{v} = 0$$
 in K .



Given a mesh \mathcal{T}_h on Ω we derive the TDGFEM as follows.

Multiply by test functions and integrate by parts, element-wise, twice (ultra weak formulation):

$$\int_{\mathcal{K}} u(-\Delta \bar{v} - k^2 \bar{v}) d\mathbf{x} + \int_{\partial \mathcal{K}} u \nabla \bar{v} \cdot \mathbf{n}_{\mathcal{K}} ds - \int_{\partial \mathcal{K}} \nabla u \cdot \mathbf{n}_{\mathcal{K}} \bar{v} ds = 0$$

Replace continuous functions by discrete approximations $(u_{hp}, v_{hp} \in V_p(\mathcal{T}_h))$ and traces by numerical fluxes

$$u \to \widehat{u}_{hp}, \qquad \nabla u \to ik\widehat{\sigma}_{hp}.$$

•
$$v \in V_p(\mathcal{T}_h) \subset T(\mathcal{T}_h) \implies -\Delta \bar{v} - k^2 \bar{v} = 0$$
 in K .

$$\int_{\partial K} \widehat{u}_{hp} \nabla \overline{v}_{hp} \cdot \boldsymbol{n}_K \, ds - \int_{\partial K} ik \widehat{\sigma}_{hp} \cdot \boldsymbol{n}_K \overline{v}_{hp} \, ds = 0, \qquad \text{for all } K \in \mathcal{T}_h.$$

.



Trefftz Discontinuous Galerkin FEM for Helmholtz

Find $u_{hp} \in V_p(\mathcal{T}_h)$ such that,

$$\mathcal{A}_h(u_{hp}, v_{hp}) = \ell_h(v_{hp}),$$

for all $v_{hp} \in V_p(\mathcal{T}_h)$, where

$$\begin{split} \mathcal{A}_{h}(u,v) &= \int_{\mathcal{F}_{h}^{l}\cup\mathcal{F}_{h}^{N}} \left\{\!\!\left\{u\right\}\!\!\right\} \left[\!\left[\nabla_{h}\bar{v}\right]\!\right] ds - \int_{\mathcal{F}_{h}^{l}\cup\mathcal{F}_{h}^{N}} \beta(ik)^{-1} \left[\!\left[\nabla_{h}u\right]\!\right] \left[\!\left[\nabla_{h}\bar{v}\right]\!\right] ds \\ &- \int_{\mathcal{F}_{h}^{l}\cup\mathcal{F}_{h}^{D}} \left\{\!\!\left\{\nabla_{h}u\right\}\!\!\right\} \cdot \left[\!\left[\bar{v}\right]\!\right] ds + \int_{\mathcal{F}_{h}^{l}\cup\mathcal{F}_{h}^{D}} \alpha ik \left[\!\left[u\right]\!\right] \cdot \left[\!\left[\bar{v}\right]\!\right] ds \\ &+ \int_{\mathcal{F}_{h}^{R}} (1-\delta) u \nabla_{h} \bar{v} \cdot \mathbf{n} \, ds - \int_{\mathcal{F}_{h}^{R}} \delta(ik\vartheta)^{-1} (\nabla_{h}u \cdot \mathbf{n}) (\nabla_{h} \bar{v} \cdot \mathbf{n}) \, ds \\ &- \int_{\mathcal{F}_{h}^{R}} \delta \nabla_{h} u \cdot \mathbf{n} \bar{v} \, ds + \int_{\mathcal{F}_{h}^{R}} (1-\delta) ik \vartheta u \bar{v} \, ds, \\ \ell_{h}(v) &= - \int_{\mathcal{F}_{h}^{R}} \delta(ik\vartheta)^{-1} g_{R} \nabla_{h} \bar{v} \cdot \mathbf{n} \, ds + \int_{\mathcal{F}_{h}^{R}} (1-\delta) g_{R} \bar{v} \, ds. \end{split}$$

Flux Parameters



Penalty Type	$ \alpha$	β	δ
DG-type Gittelson, Hiptmair & Perugia, 2009	aq_K^2/kh_K	ъkh _K /q _K	₫ <i>kh_K/q_K</i>
Constant Hiptmair, Moiola & Perugia, 2011	a	b	d
UWVF Cessenat & Després, 1998	1/2	1/2	1/2
Non-Uniform Mesh Hiptmair, Moiola & Perugia, 2014	ah_{max}/h_K	b <i>h</i> max/ <i>h</i> K	dh_{max}/h_K

For the rest of this talk we ignore Neumann boundary conditions.

Flux Parameters



Penalty Type	α	β	δ
DG-type Gittelson, Hiptmair & Perugia, 2009	aq_K^2/kh_K	ъkh _K /q _K	₫ <i>kh_K/q_K</i>
Constant Hiptmair, Moiola & Perugia, 2011	a	b	d
UWVF Cessenat & Després, 1998	1/2	1/2	1/2
Non-Uniform Mesh Hiptmair, Moiola & Perugia, 2014	ah_{max}/h_K	bh _{max} /h _K	dh_{max}/h_K

For the rest of this talk we ignore Neumann boundary conditions.

Energy Norm

$$\begin{aligned} \| \mathbf{v} \|_{\mathrm{TDG}}^{2} &= k \left\| \alpha^{1/2} \left[\! \left[\mathbf{v} \right] \! \right] \right\|_{L^{2}(\mathcal{F}_{h}^{l} \cup \mathcal{F}_{h}^{D})}^{2} + \frac{1}{k} \left\| \beta^{\frac{1}{2}} \left[\! \left[\nabla \mathbf{v} \right] \! \right] \right\|_{L^{2}(\mathcal{F}_{h}^{l})}^{2} \\ &+ \frac{1}{k\vartheta} \left\| \delta^{1/2} \nabla \mathbf{v} \cdot \mathbf{n}_{K} \right\|_{L^{2}(\mathcal{F}_{h}^{R})}^{2} + k\vartheta \left\| (1-\delta)^{1/2} \mathbf{v} \right\|_{L^{2}(\mathcal{F}_{h}^{R})}^{2} \end{aligned}$$

A priori Error Estimates



Define the weighted Sobolev norm

$$\|v\|_{H^{s}(\Omega),k} = \sum_{j=0}^{s} k^{2(s-j)} |v|^{2}_{H^{j}(\Omega)}.$$

Theorem (*a priori* — Non-Uniform Mesh & Non-Uniform Parameters)

Let u be the analytical solution with $u|_{K} \in H^{s_{K}+1}(K)$, u_{hp} the TDG solution. For sufficiently large q_{K} (and assuming $q_{K} > 2s_{K} + 1$)

$$\begin{split} \|u-u_{\rho}\|_{L^{2}(\Omega)} &\leq Cd_{\Omega}^{2}[(d_{\Omega}k)^{-1} + (d_{\Omega}^{-1}h)^{s_{\kappa}+1/2}] \\ &\times \sum_{K\in\mathcal{T}_{h}}C_{K}h_{K}^{s_{\kappa}-1}\left(\frac{1}{\widehat{q}_{\kappa}}\right)^{s_{\kappa}-1/2}\|u\|_{H^{s+1}(\Omega),k}, \end{split}$$

where C_K depends on kh_K (as an increasing function) and s_K . Here, $\hat{q}_K = q_K/log(q_k+2)$. [Hiptmair, Moiola & Perugia, 2014]

Comparison of Flux Parameters (2D)



Consider the smooth (analytic) solution (for Acoustic Wave Propagation)

 $u(r,\theta) = \mathcal{J}_1(kr)\cos(\theta)$

on the domain $\Omega = (0,1) \times (-1/2,1/2)$.



Re(Anal. Soln.) (k=20)

Comparison of Flux Parameters (2D)



Consider the smooth (analytic) solution (for Acoustic Wave Propagation)

 $u(r,\theta) = \mathcal{J}_1(kr)\cos(\theta)$

on the domain $\Omega=(0,1)\times(-^{1\!\!/2},^{1\!\!/2}).$

We solve using constant (solid line) and DG-type parameters (dashed).







To test the non-uniform parameters, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{x^2+y^2}),$$

with k = 50, on the domain $\Omega = (0, 1)^2$, where $\mathcal{H}_0^{(1)}$ represents the Hankel function of the first kind of order 0.



Im(Anal. Soln.)



To test the non-uniform parameters, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{x^2+y^2}),$$

with k = 50, on the domain $\Omega = (0, 1)^2$, where $\mathcal{H}_0^{(1)}$ represents the Hankel function of the first kind of order 0.



Mesh 1



To test the non-uniform parameters, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{x^2+y^2}),$$

with k = 50, on the domain $\Omega = (0, 1)^2$, where $\mathcal{H}_0^{(1)}$ represents the Hankel function of the first kind of order 0.



Mesh 2



To test the non-uniform parameters, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{x^2+y^2}),$$

with k = 50, on the domain $\Omega = (0, 1)^2$, where $\mathcal{H}_0^{(1)}$ represents the Hankel function of the first kind of order 0.





To test the non-uniform parameters, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{x^2+y^2}),$$

with k = 50, on the domain $\Omega = (0, 1)^2$, where $\mathcal{H}_0^{(1)}$ represents the Hankel function of the first kind of order 0.





To test the non-uniform parameters, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{x^2+y^2}),$$

with k = 50, on the domain $\Omega = (0, 1)^2$, where $\mathcal{H}_0^{(1)}$ represents the Hankel function of the first kind of order 0.





To test the non-uniform parameters, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{x^2+y^2}),$$

with k = 50, on the domain $\Omega = (0, 1)^2$, where $\mathcal{H}_0^{(1)}$ represents the Hankel function of the first kind of order 0.



Mesh 6
Comparison of Flux Parameters (Non-Unif.)



To test the non-uniform parameters, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{x^2+y^2}),$$

with k = 50, on the domain $\Omega = (0, 1)^2$, where $\mathcal{H}_0^{(1)}$ represents the Hankel function of the first kind of order 0.



Comparison of Flux Parameters (Non-Unif.)



To test the non-uniform parameters, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{x^2+y^2}),$$

with k = 50, on the domain $\Omega = (0, 1)^2$, where $\mathcal{H}_0^{(1)}$ represents the Hankel function of the first kind of order 0.



Scott Congreve (Universität Wien)

hp-TDGFEM for Helmholtz



Consider a plane wave analytical solution (for Acoustic Wave Propagation)

$$u(\mathbf{x}) = e^{ik\mathbf{d}\cdot\mathbf{x}}$$

for k=20 on the domain $\Omega=(0,1)^2$, where ${\pmb d}=(1/\sqrt{2},1/\sqrt{2}).$



Consider a plane wave analytical solution (for Acoustic Wave Propagation)

$$u(\mathbf{x}) = e^{ik\mathbf{d}\cdot\mathbf{x}}$$

for k = 20 on the domain $\Omega = (0, 1)^2$, where $\boldsymbol{d} = (1/\sqrt{2}, 1/\sqrt{2})$. We evenly distribute directions \boldsymbol{d}_{ℓ} , starting from $\boldsymbol{d}_1 = (1, 0)$.





Consider a plane wave analytical solution (for Acoustic Wave Propagation)

$$u(\boldsymbol{x}) = \mathrm{e}^{ik\boldsymbol{d}\cdot\boldsymbol{x}}$$

for k = 20 on the domain $\Omega = (0, 1)^2$, where $\boldsymbol{d} = (1/\sqrt{2}, 1/\sqrt{2})$. We evenly distribute directions \boldsymbol{d}_{ℓ} , starting from $\boldsymbol{d}_1 = (1, 0)$.

Rotating directions so that $d_1 = d$ (almost) gives the analytical solution.







We need a way calculate/adapt the directions without the analytical solution. Several existing approaches exist:

- Ray-tracing requires a source term. [Betcke & Phillips, 2012]
- Approximate

$$\frac{\nabla e(\boldsymbol{x}_0)}{ike(\boldsymbol{x}_0)},$$

where e is the error. [Gittelson, 2008 (Master's Thesis)]

 Adding an extra unknown (the optimal angle of rotation) to the basis functions. [Amara, Chaudhry, Diaz, Djellouli & Fiedler, 2014]



We need a way calculate/adapt the directions without the analytical solution. Several existing approaches exist:

- Ray-tracing requires a source term. [Betcke & Phillips, 2012]
- Approximate

$$\frac{\nabla e(\boldsymbol{x}_0)}{ike(\boldsymbol{x}_0)},$$

where e is the error. [Gittelson, 2008 (Master's Thesis)]

 Adding an extra unknown (the optimal angle of rotation) to the basis functions. [Amara, Chaudhry, Diaz, Djellouli & Fiedler, 2014]

We propose using the Hessian of the numerical solution, based on work on anisotropic meshes for standard FE [Formaggia & Perotto, 2001, 2003].



We need a way calculate/adapt the directions without the analytical solution. Several existing approaches exist:

- Ray-tracing requires a source term. [Betcke & Phillips, 2012]
- Approximate

$$\frac{\nabla e(\boldsymbol{x}_0)}{ike(\boldsymbol{x}_0)},$$

where e is the error. [Gittelson, 2008 (Master's Thesis)]

 Adding an extra unknown (the optimal angle of rotation) to the basis functions. [Amara, Chaudhry, Diaz, Djellouli & Fiedler, 2014]

We propose using the Hessian of the numerical solution, based on work on anisotropic meshes for standard FE [Formaggia & Perotto, 2001, 2003]. The eigenvector of the Hessian matching the largest eigenvalue should be the direction to use as the main direction, assuming the matching eigenvalue is significantly larger.

Scott Congreve (Universität Wien)

hp-TDGFEM for Helmholtz



Plane Wave Refinement Algorithm (2D)

Let $(\lambda_1, \mathbf{v}_1), (\lambda_2, \mathbf{v}_2)$ be the eigenpairs of $\mathbf{H}(\operatorname{Re}(u_h(\mathbf{x}_K)))$, and $(\mu_1, \mathbf{w}_1), (\mu_2, \mathbf{w}_2)$ the eigenpairs of $\mathbf{H}(\operatorname{Im}(u_h(\mathbf{x}_K)))$ s.t. $\lambda_1 \ge \lambda_2$, $\mu_1 \ge \mu_2$; then, for constant C > 1, we can select the first plane wave direction as follows:

$\lambda_1 \ge C\lambda_2$	$\mu_1 \ge C\mu_2$	$\lambda_1 \geq C\mu_1$	$\mu_1 \geq C\lambda_1$	First PW Direction
✓	1	1	×	v ₁
1	1	×	1	w ₁
1	1	×	×	$(v_1+w_1)/2$
1	×	1	X	v ₁
1	×	×	-	-
×	1	×	1	w ₁
×	1	-	×	-
×	X	_	_	-









Evaluating at $\mathbf{x}_{\mathcal{K}} + \delta \mathbf{v}$ we note that the normal is \mathbf{v} , so we can calculate

$$\frac{\nabla u_h(\boldsymbol{x}_K) \cdot \boldsymbol{v} + iku_h(\boldsymbol{x}_K)}{iku_h(\boldsymbol{x}_K)}$$





Evaluating at $\mathbf{x}_{\mathcal{K}} + \delta \mathbf{v}$ we note that the normal is \mathbf{v} , so we can calculate

$$\frac{\nabla u_h(\boldsymbol{x}_K) \cdot \boldsymbol{v} + iku_h(\boldsymbol{x}_K)}{iku_h(\boldsymbol{x}_K)}$$

We can compare this to the impedance for the *u*:

$$\frac{\nabla u(\boldsymbol{x}_{K}) \cdot \boldsymbol{v} + iku(\boldsymbol{x}_{K})}{iku(\boldsymbol{x}_{K})} = \begin{cases} 2, & \text{if } \boldsymbol{d} = \boldsymbol{v}, \end{cases}$$





Evaluating at $\mathbf{x}_{K} + \delta \mathbf{v}$ we note that the normal is \mathbf{v} , so we can calculate

$$\frac{\nabla u_h(\boldsymbol{x}_K) \cdot \boldsymbol{v} + iku_h(\boldsymbol{x}_K)}{iku_h(\boldsymbol{x}_K)}$$

We can compare this to the impedance for the *u*:

$$\frac{\nabla u(\boldsymbol{x}_{K}) \cdot \boldsymbol{v} + iku(\boldsymbol{x}_{K})}{iku(\boldsymbol{x}_{K})} = \begin{cases} 2, & \text{if } \boldsymbol{d} = \boldsymbol{v}, \\ 0, & \text{if } \boldsymbol{d} = -\boldsymbol{v}. \end{cases}$$



To test the direction refinement, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{(x+0.25)^2+y^2}),$$





To test the direction refinement, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{(x+0.25)^2+y^2}),$$





To test the direction refinement, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{(x+0.25)^2+y^2}),$$





To test the direction refinement, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{(x+0.25)^2+y^2}),$$





To test the direction refinement, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{(x+0.25)^2+y^2)},$$





To test the direction refinement, we consider the solution

$$u(x,y) = \mathcal{H}_0^{(1)}(k\sqrt{(x+0.25)^2+y^2}),$$





Ignoring Neumann boundary conditions *a posteriori* error bounds exists for the *h*-version of the method in \mathbb{R}^2 .

A posteriori Error Estimates



Ignoring Neumann boundary conditions *a posteriori* error bounds exists for the *h*-version of the method in \mathbb{R}^2 .

A posteriori Error Bound — h-version Only

For the TDGFEM, with the non-uniform flux parameters, the following error bound holds:

$$\begin{aligned} \|u - u_{hp}\|_{L^{2}(\Omega)} &\leq C \left\{ \left\| \alpha^{1/2} h_{F}^{s} \llbracket u_{h} \rrbracket \right\|_{L^{2}(\mathcal{F}_{h}^{l} \cup \mathcal{F}_{h}^{D})} + \frac{1}{k} \|\beta^{\frac{1}{2}} h_{F}^{s} \llbracket \nabla u_{h} \rrbracket \|_{L^{2}(\mathcal{F}_{h}^{l})} \\ &+ \frac{1}{k} \left\| \delta^{1/2} h_{F}^{s} \left(g_{R} - \nabla u_{h} \cdot \boldsymbol{n}_{K} + ik\vartheta u_{h} \right) \right\|_{L^{2}(\mathcal{F}_{h}^{R})} \right\} \end{aligned}$$

where s depends on the regularity of the solution to the adjoint problem $(z \in H^{3/2+s}(\Omega)).$

[Kapita, Monk, Warburton (2014 - Tech. Report)]



Consider again the solution

$$u(x,y) = H_0^{(1)}(k(x^2 + y^2)),$$

with k = 50, on the domain $\Omega = (0, 1)^2$. We solve using constant (solid line), DG-type (dashed) and non-uniform parameter (dotted).



Scott Congreve (Universität Wien)



Consider again the solution

$$u(x,y) = H_0^{(1)}(k(x^2 + y^2)),$$

with k = 50, on the domain $\Omega = (0, 1)^2$. We solve using constant (solid line), DG-type (dashed) and non-uniform parameter (dotted).



y 2016 21 / 22



Consider again the solution

$$u(x,y) = H_0^{(1)}(k(x^2 + y^2)),$$





Consider again the solution

$$u(x,y) = H_0^{(1)}(k(x^2 + y^2)),$$





Consider again the solution

$$u(x,y) = H_0^{(1)}(k(x^2 + y^2)),$$





Consider again the solution

$$u(x,y) = H_0^{(1)}(k(x^2 + y^2)),$$





Consider again the solution

$$u(x,y) = H_0^{(1)}(k(x^2 + y^2)),$$





Summary:

A priori results exist for Trefftz DG, with Robin and Dirichlet BCs



Summary:

- A priori results exist for Trefftz DG, with Robin and Dirichlet BCs
- Various choice of flux parameters is required for the existing analysis



Summary:

- A priori results exist for Trefftz DG, with Robin and Dirichlet BCs
- Various choice of flux parameters is required for the existing analysis
- The choice of flux parameters tends to make no difference on smooth solutions, although DG-style parameters appear poor for non-uniform refinement/singular problems.



Summary:

- A priori results exist for Trefftz DG, with Robin and Dirichlet BCs
- Various choice of flux parameters is required for the existing analysis
- The choice of flux parameters tends to make no difference on smooth solutions, although DG-style parameters appear poor for non-uniform refinement/singular problems.
- With plane wave basis functions it is possible to refine the wave directions.



Summary:

- A priori results exist for Trefftz DG, with Robin and Dirichlet BCs
- Various choice of flux parameters is required for the existing analysis
- The choice of flux parameters tends to make no difference on smooth solutions, although DG-style parameters appear poor for non-uniform refinement/singular problems.
- With plane wave basis functions it is possible to refine the wave directions.

Future Aims:



Summary:

- A priori results exist for Trefftz DG, with Robin and Dirichlet BCs
- Various choice of flux parameters is required for the existing analysis
- The choice of flux parameters tends to make no difference on smooth solutions, although DG-style parameters appear poor for non-uniform refinement/singular problems.
- With plane wave basis functions it is possible to refine the wave directions.

Future Aims:

 Extend the existing a posteriori error analysis to hp-version meshes (ideally for constant flux parameters).



Summary:

- A priori results exist for Trefftz DG, with Robin and Dirichlet BCs
- Various choice of flux parameters is required for the existing analysis
- The choice of flux parameters tends to make no difference on smooth solutions, although DG-style parameters appear poor for non-uniform refinement/singular problems.
- With plane wave basis functions it is possible to refine the wave directions.

Future Aims:

- Extend the existing a posteriori error analysis to hp-version meshes (ideally for constant flux parameters).
- Develop an algorithm for deciding on whether to perform h or p refinement.
Conclusion



Summary:

- A priori results exist for Trefftz DG, with Robin and Dirichlet BCs
- Various choice of flux parameters is required for the existing analysis
- The choice of flux parameters tends to make no difference on smooth solutions, although DG-style parameters appear poor for non-uniform refinement/singular problems.
- With plane wave basis functions it is possible to refine the wave directions.

Future Aims:

- Extend the existing a posteriori error analysis to hp-version meshes (ideally for constant flux parameters).
- Develop an algorithm for deciding on whether to perform h or p refinement.
- Use the eigenvalues/eigenvectors to develop anisotropic p-refinement (unevenly spaced plane waves).