

New Perspectives in Modeling Non-Newtonian Fluids

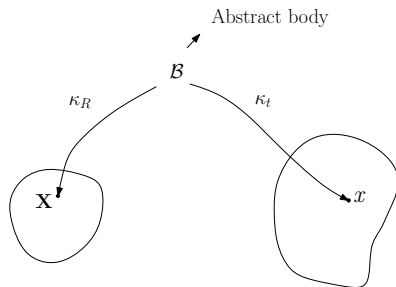
K. R. Rajagopal

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– E. Mach
- In the presentation of a novel outlook with wide ramifications a single line of communication from premises to conclusions is not sufficient for intelligibility. Your audience will construe whatever you say in conformity with pre-existing outlook.
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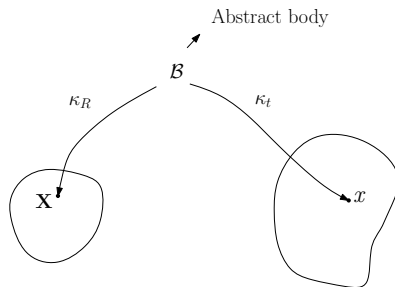
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- κ_R, κ_t – placers
- $\kappa_R(\mathcal{B}), \kappa_t(\mathcal{B})$ – configurations
- Motion: One-parameter family of placers.

$$\boldsymbol{x} = \chi_{\kappa_R}(\boldsymbol{X}, t). \quad (1)$$

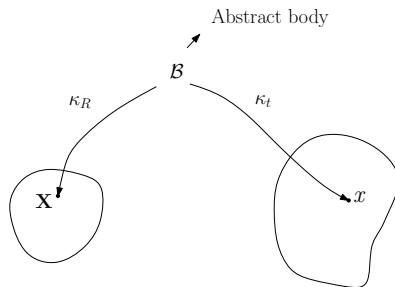
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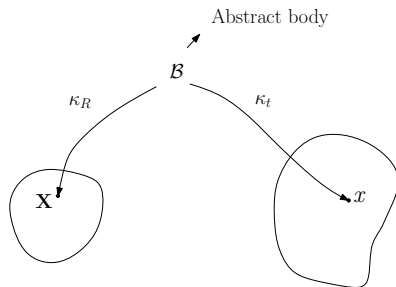
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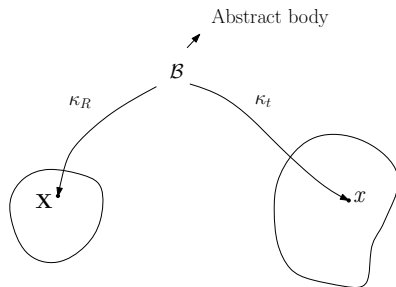
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- Relative Motion

$$\xi := \chi_{\kappa_R} (\chi_{\kappa_R}^{-1}(\mathbf{x}, t), \tau) = \chi_t(\mathbf{x}, \tau). \quad (2)$$

- Deformation Gradient

$$\mathbf{F}_{\kappa_R} := \frac{\partial \chi_{\kappa_R}}{\partial \mathbf{X}} \quad (3)$$

(An unnecessary and ill-conceived concept).

- \mathbf{F}_{κ_R} is a linear transformation from the tangent space at \mathbf{X} to the tangent space at \mathbf{x} .
- Relative Deformation Gradient

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- Classical Cauchy Elasticity

$$\mathbf{T} = \mathbf{f}_{\kappa_R}(\mathbf{F}_{\kappa_R}). \quad (9)$$

- Classical Navier Stokes Fluid

$$\begin{aligned} \mathbf{T} &= -p(\rho_{\kappa_t})\mathbf{I} + \lambda(\rho_{\kappa_t})(\text{tr}\mathbf{D}_{\kappa_t})\mathbf{I} + 2\mu\mathbf{D}_{\kappa_t}, \quad (10) \\ \mathbf{D}_{\kappa_t} &= \frac{1}{2} \left[\nabla_{\mathbf{x}}\mathbf{v} + (\nabla_{\mathbf{x}}\mathbf{v})^T \right] \end{aligned}$$

- ρ_{κ_t} – density, p – thermodynamic pressure
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- There is only one stress-free configuration modulo rigid motion.
- The stress is completely known from a single kinematical measurement from a single configuration.

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- Tacit assumption that

$$\mathbf{f}_{\kappa_t} = \mathbf{f} \quad \forall t \in \mathbb{R}. \quad (13)$$

- However, possible that

$$\mathbf{T} = \begin{cases} -p_1 \mathbf{I} + 2\mu_1 \mathbf{D}_{\kappa_t} & \forall t \leq t' \\ -p_2 \mathbf{I} + 2\mu_2 \mathbf{D}_{\kappa_t} + 2\mu_3 \mathbf{D}_{\kappa_t}^2 & \forall t \geq t' \end{cases} \quad (14)$$

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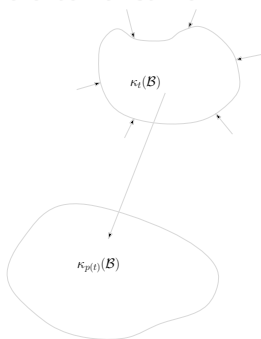
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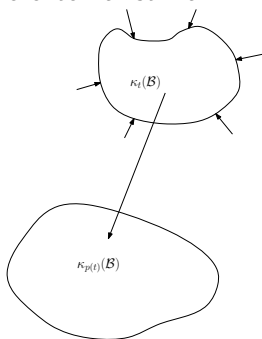
- “Natural Configuration” – The configuration the body takes on the removal of the external stimuli.



- $\kappa_{p(t)}(\mathcal{B})$ – preferred natural configuration associated with the configuration $\kappa_t(\mathcal{B})$.
 - depends on the process class that is allowed.
- The symmetry of the body in the natural configurations can be different.

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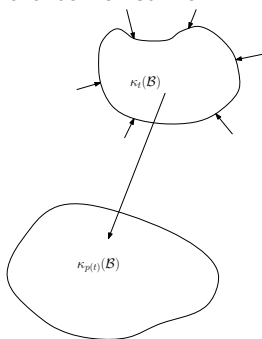
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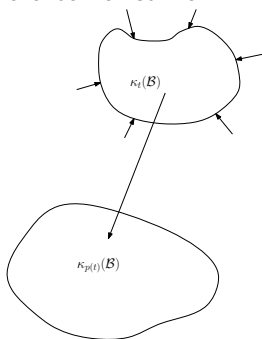
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Notion of “Natural Configuration”

- A body is not necessarily a fixed set of particles – Growth and Adaptation of biological bodies.
- To define a “Body”, it is necessary to know the natural configurations a body is capable of existing in. In any process, we need to know which natural configurations are accessed.
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Notion of “Natural Configuration”

- The same piece of steel can undergo
 - a non-dissipative process
 - twinning
 - slip
 - solid to solid phase transformation
 - melting
 - etc.
- We need to define “states”, “processes”, “process classes” : Isothermal, Adiabatic, Isentropic, Isenthalpic, Isobaric, Isotonic, etc.
- Different natural configurations are accessed during different processes. The “natural configuration” is a part of the specification of the “state” of the body.

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- If one inhomogeneously deforms a body and then removes the traction, it is possible that the unloaded body will not fit together compatibly and be simultaneously stress free in an Euclidean Space.
- However, it can be unloaded to fit together in a non-Euclidean space in which it is stress-free (Eckart - 1940s).
- A “sufficiently small” neighborhood of a material point can be unloaded to a stress-free configuration. Here, “sufficiently small” corresponds to a neighborhood in which the deformation is “essentially homogeneous”.
- Henceforth, we will assume, for the sake of illustration the deformation is homogeneous.

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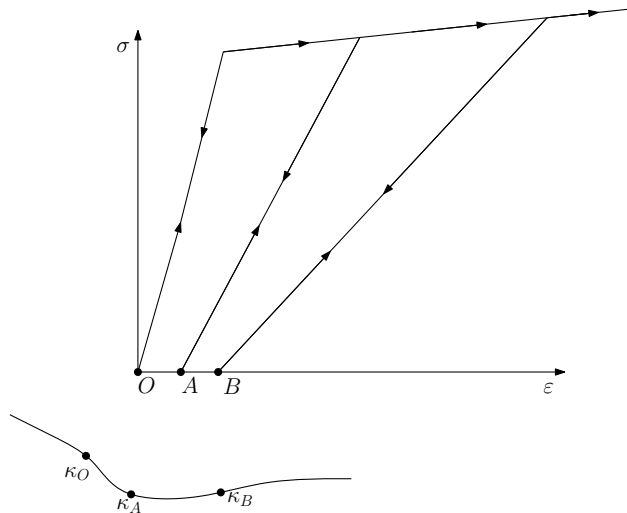
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Natural Configuration in Traditional Plasticity



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 - Classical Elastic Body
- A body can have a finite number of natural configurations.
 - Twinning, Solid to Solid phase transition
- A body can have infinity of natural configurations.
 - Classical Fluid
 - Traditional Plasticity
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$$\frac{\partial \rho}{\partial t} + \operatorname{div}(\rho \mathbf{v}) = 0. \quad (15)$$

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$$\rho \frac{d\mathbf{v}}{dt} = \operatorname{div}(\mathbf{T}^T) + \rho \mathbf{b}. \quad (16)$$

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ϵ – specific internal energy

\mathbf{q} – heat flux vector

r – radiant heating

$\mathbf{L} = \nabla_{\mathbf{x}} \mathbf{v}$.

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$$\rho \frac{d\eta}{dt} + \operatorname{div} \left(\frac{\mathbf{q}}{\theta} \right) - \frac{\rho r}{\theta} = \rho \xi \geq 0. \quad (19)$$

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- Can generalize Onsager's linear phenomenological laws to non-linear cases.
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